

# Low-temperature sintering of sodium beta alumina ceramics using nanosized SnO<sub>2</sub> sintering aid

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## Abstract

Sodium beta alumina ceramics ( $Na_{1.67}Al_{10.67}Li_{0.33}O_{17}$ ) is used in sodium sulphur batteries as solid electrolyte. In the present work, sodium beta alumina powder has been synthesized by the solid state method using  $Al_2O_3$ ,  $Na_2CO_3$  and  $Li_2CO_3$  as the starting materials. The effect of nanosized  $SnO_2$  additive on sintering behaviour, microstructure, mechanical and electrical properties of sodium beta alumina ceramics has been investigated. The results indicated that the addition of 1 mol% of nanosized  $SnO_2$  particles, determined as the optimal amount, can decrease the sintering temperature of sodium beta alumina ceramics for about 100 °C, and lead to the excellent densification and proper microstructure, as well. Improvement in sintering behaviour of beta alumina ceramics in the presence of nanosized  $SnO_2$  additive is apparently due to the formation of a liquid phase during the sintering process and lower sodium loss. The results also proved that by  $SnO_2$  addition, ionic conductivity at 300 °C, fracture strength and Weibull modulus of the sintered samples are improved by 66%, 58%, and 45%, respectively. These improvements could be attributed to the higher amount of  $\beta''-Al_2O_3$  phase, higher density and more uniform microstructure.

Keywords: sodium beta alumina, nanosized SnO<sub>2</sub>, sintering, mechanical properties, ionic conductivity

## I. Introduction

The engineering properties of ceramics are strongly dependent on the microstructural features, including size and shape of the grains, amount of remained porosity, pore size and the distribution of pores in the fired body. For most applications, microstructural control usually means achievement of the high density, small grain size and homogeneous microstructure [1]. Using sintering aids is a well known method for altering microstructure during sintering of ceramic materials which could modify densification characteristics and improve mechanical, magnetic and electrical properties of the fired sample [2-6]. In recent years, it has been shown that using sintering aids with nanoparticle size can reduce the required amount of sintering aids even down to 1 mol% and can also improve properties of the sintered products [7–13]. The unique properties of nanoparticles are primarily due to their large surface-to-volume ratio and their high activity.

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Sodium beta alumina ceramics has been studied widely because of their application as solid electrolyte in sodium sulphur and ZEBRA batteries [14–16]. However, it is very difficult to obtain dense and well-sintered sodium beta alumina ceramics using an ordinary sintering process because of the high volatility of alkaline elements at high temperatures [16–18]. The sintering temperature of sodium beta alumina ceramics is generally higher than 1600 °C [19-21]. The volatilization of sodium at high sintering temperature and the poor densities at low sintering temperature are deleterious to mechanical strength and ionic conductivity of this electrolyte [16]. It would be possible to lower the sintering temperature and overcome the mentioned difficulties by using sintering aids. The effects of different sintering aids including ZnO, MgO, Nb2O3, Sm2O3 and nano-CuO on the densification behaviour and properties of sodium beta alumina electrolyte have been investigated [6, 22-24].

In the present work, the effects of the nanosized  $\text{SnO}_2$  additive as a sintering aid on sinterability, microstructure, mechanical and electrical properties of sodium

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beta alumina ceramics, synthesized by the solid state method, have been investigated.

#### **II. Experimental procedure**

#### 2.1. Synthesis method

Sodium beta alumina was synthesized by the solid state method. In this method, the starting materials were: Na<sub>2</sub>CO<sub>3</sub> and Li<sub>2</sub>CO<sub>3</sub> (with 99.9% purity from Carlo Erba Company) and  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> (with 99.9% purity from Inframat Advanced Materials Company). According to the chemical formula of Li2O-stabilized  $\beta''$ -alumina as Na<sub>1.67</sub>Al<sub>10.67</sub>Li<sub>0.33</sub>O<sub>17</sub>, stoichiometric amounts of the starting materials were first weighed, intimately mixed and calcined at 1300 °C for 2 h. High purity nanosized SnO<sub>2</sub> powder (99.9%, ≤80 nm, Advanced Materials US) was used as sintering aids. Required amount of the nanosized SnO<sub>2</sub> (i.e. 0.5, 1 and 2 mol%) was mixed with the calcined powder by attrition milling using 5 mm zirconia balls in the ethanol medium for 4 h with the fixed rotation speed of 480 rpm. After the slurries were dried, the powder was granulated by passing through 60 mesh number screen and shaped in a die by applying 200 MPa pressure uniaxially. Disk shaped samples with a thickness of 2 mm and diameter of 12 mm were fired at different temperatures including 1520, 1570 and 1620 °C for 15 min with the heating rate of 4 °C/min. In order to minimize sodium loss, the green samples were placed in an alumina-crucible and covered with the  $\beta''$ -alumina powder.

#### 2.2. Characterization techniques

The density of the sintered samples was measured by the Archimedes' method in ethanol as an immersion medium. Phase purity of the sintered samples was examined by a BRUKER X-ray diffractometer using Cu K $\alpha$  radiation. The scans of the selected diffraction peaks were carried out in the step mode (step size of 0.05°, measurement time of 5 s). Relative phase fractions of  $\beta$ -Al<sub>2</sub>O<sub>3</sub> ( $f(\beta)$ ) and  $\beta''$ -Al<sub>2</sub>O<sub>3</sub> ( $f(\beta'')$ ) were calculated according to the Pekarsky's formula as follows [25]:

$$f(\beta'') = 100 - f(\beta) = 100 - \frac{1.14I_{\beta}}{1.14I_{\beta} + I_{\beta''}} \qquad (1)$$

where  $I_{\beta}$  and  $I_{\beta''}$  are peak intensities of  $\beta$  and  $\beta''$  phase at 44.50° and 45.90°, respectively.

The microstructure of the sintered samples was characterized by scanning electron microscope (SEM, Leica Cambridge S360). For the SEM observations, the specimens were polished to a mirror finish and then thermally etched at 100 °C lower than used sintering temperature for 30 min in air. In this study, biaxial flexure test (BFT) was used to evaluate the mechanical strength of the sintered samples. In this experiment, load is applied by a loading ring on the disc specimen that is placed on a supporting ring (this test is also termed "ring on ring" and is carried out under the ASTM C1499, 2003 standard). In the present work the variability in fracture strength values was analysed according to two parameters proposed in the Weibull approach [26]. The ionic conductivity of the sintered ceramics was measured by AC 2-probe impedance analysis on a frequency response analyser (Solartron 1260, Solartron Analytical) over a frequency range of 10 Hz to 5 MHz with the symmetric platinum electrodes in the temperature range from 200 to 500 °C with 50 °C interval in air.

### III. Results and discussion

Figure 1 shows the relative densities of the fired samples as a function of the sintering temperature and amount of the used nanosized SnO<sub>2</sub> powder as sintering aid. According to these results, the density of all samples increased with sintering temperature as well as with addition of SnO<sub>2</sub>. At sintering temperature of 1620 °C, the density of the pure samples was  $3.15 \text{ g/cm}^3$ , i.e. 96.5% TD (theoretical density is  $3.26 \text{ g/cm}^3$ ) and it was increased to 99.4% TD by the addition of 1 mol% of  $SnO_2$ . The addition of 0.5 mol% of nanosized  $SnO_2$  had no significant effect on the sample densities. In contrast, using 1 mol% of nanosized SnO<sub>2</sub> additive effectively decreased sintering temperature and improved sinterability of the parent phase. The density of the sample prepared with 1 mol% of SnO<sub>2</sub> and sintered at 1520 °C was 98.1% TD, which is higher than the density of the pure sample sintered at even 100 °C higher temperature (1620 °C). Thus, it can be concluded that the addition of 1 mol% nanosized SnO<sub>2</sub> decreases the sintering temperature of sodium beta alumina ceramics for about 100 °C. Using lower sintering temperature definitely can lead to the lower sodium loss that would cause improvement in properties of sodium beta alumina ceramics [16]. Some improvement of the sintering behaviour was observed for the samples with 2 mol% of nanosized SnO<sub>2</sub>, but not as pronounced as when just 1 mol% of nanosized SnO<sub>2</sub> was added.



Figure 1. Relative densities as a function of sintering temperature and SnO<sub>2</sub> amount



Figure 2. X-ray diffraction patterns of the samples prepared with different amounts of nanosized SnO<sub>2</sub> additive

Figure 2 shows the typical X-ray diffraction patterns of the samples sintered at 1620 °C which confirms the presence of Na<sub>1.67</sub>Al<sub>10.67</sub>Li<sub>0.33</sub>O<sub>17</sub> crystalline phase [6,27]. According to XRD patterns, no impurity phases have been detected for the samples prepared with 0.5 and 1 mol% of nanosized SnO<sub>2</sub>. However, when the amount of SnO<sub>2</sub> increased to 2 mol%, a few unknown diffraction peaks were detected. So, it is proposed that, for the samples with 0.5 and 1 mol% of nanosized SnO<sub>2</sub>, Sn<sup>4+</sup> can be incorporated into the sodium beta alumina crystal lattice [6]. Decrease in the density of the sample by increasing amount of SnO<sub>2</sub> from 1 to 2 mol% can also be attributed to the presence of impurity phase in this sample.  $\beta$ -Al<sub>2</sub>O<sub>3</sub> (hexagonal) and  $\beta''$ -Al<sub>2</sub>O<sub>3</sub> (rhombohedral) are two main subgroups of sodium beta alumina and  $\beta''$ -Al<sub>2</sub>O<sub>3</sub> exhibits a significantly higher ionic conductivity than  $\beta$ -Al<sub>2</sub>O<sub>3</sub> [16]. The amount of  $\beta''$ -Al<sub>2</sub>O<sub>3</sub> was calculated using Eq. 1 and it is 99% in the sample with 1 mol% of nano SnO<sub>2</sub>, which is about 4%

higher than that of the pure sample. The effect of cation additives in sodium beta alumina depends on their size and charge. The oxygen atoms in the spinel block portion of the structure are closely packed with small  $Al^{3+}$ ions in the interstices. Al<sup>3+</sup> ions can be replaced by small cations without undue strain [28]. According to the Boilot and Thery's theory, as the ionic radius of Sn<sup>4+</sup> cation (0.071 nm) is smaller than 0.097 nm of  $Al^{3+}$ ,  $Sn^{4+}$ is able to occupy  $Al^{3+}$  positions in the spinel block in the way to stabilize the structure of  $\beta''$ -Al<sub>2</sub>O<sub>3</sub> phase [24,29]. Regarding the densities and XRD results, it can be concluded that the optimal amount of  $SnO_2$  was  $1 \mod \%$ . Therefore, in further research the properties of the sample with 1 mol% of nanosized SnO<sub>2</sub>, sintered at 1520 °C, are compared with the properties of the pure sample sintered at 1620 °C.

Figure 3 shows SEM micrographs of the crosssection of the sintered samples. As it can be seen, the pure sample contains few pores. The dense microstruc-



Figure 3. Cross-section SEM micrographs of the sodium beta alumina: a) pure sample sintered at 1620 °C and b) sample prepared with 1 mol% of nanosized SnO<sub>2</sub> additive sintered at 1520 °C

ture with no pores or cracks, observed for the ceramics prepared with 1 mol% of nanosized SnO<sub>2</sub> additive, was confirmation of higher density even at lower sintering temperature. The existence of SnO<sub>2</sub> could improve the densification behaviour of sodium beta alumina ceramics in virtue of lower sodium loss and formation of a liquid phase during the sintering process [11,22]. In liquidphase sintering, the additive melts or reacts with a small part of the major component to form an eutectic liquid. The formation of the liquid phase by melting of the additive is fairly common in metallic systems, whereas, the formation of an eutectic liquid is more common in ceramics [1]. The liquid phase sintering with the addition of nanosized SnO<sub>2</sub> could be attributed to the formation of Li<sub>2</sub>SnO<sub>2</sub> and Li<sub>8</sub>SnO<sub>6</sub> phases with a lower melting point then the sintering temperature. According to the PDF files of X'Pert High Score software (PDF# 00-31-0761 and 00-024-0659), the XRD main peaks of these phases could be matched to the crystalline phase of  $Na_{1.67}Al_{10.67}Li_{0.33}O_{17}$  [30,31]. The presence of these phases could improve the densification of sodium beta alumina ceramics in virtue of the formation of the liquid phase during the sintering process.

Advanced ceramics must meet very specific property requirements and therefore their microstructure must be well controlled [26]. Disadvantages of the solid state process include sodium loss and exaggerated grain growth during the high-temperature sintering [16]. SEM images of the sintered and thermally etched samples are shown in Fig. 4. These images demonstrate that the addition of nanosized SnO<sub>2</sub> causes changes in the microstructure. The pure sample shows typical duplex microstructure consisting of large grains in a fine-grained matrix. However, for the sample prepared with 1 mol% of nanosized SnO<sub>2</sub> additive more uniform microstructure has been created. As it can be recognized, the small amount of nanosized SnO2 additive could promote sintering of sodium beta alumina ceramics and effectively restrict the grain growth at the same time. The formation of liquid phases and the inhibition of grain growth together improve densification of sodium beta alumina [32].

The strength is strongly affected by microstructure (e.g. porosity and grain size). The extensive grain growth can lead to a significant reduction in mechanical properties. The strength of sodium beta alumina



Figure 4. SEM micrographs of thermally etched pure sample sintered at 1620 °C (a, b) and sample prepared with 1 mol% of nanosized SnO<sub>2</sub> additive sintered at 1520 °C (c, d)



Figure 5. Two-parameter Weibull plot of the fracture strength

ceramics with a duplex structure varies from 120 to 170 MPa, depending on the size and amount of large grains in the matrix [16]. In the present work biaxial flexure test was applied to 15 samples for each composition. The average fracture strength of the sample prepared with 1 mol% of nanosized SnO<sub>2</sub> additive exceeded 198  $\pm$  16 MPa, while the fracture strength of the pure sample was only  $125 \pm 21$  MPa. The results of other researchers confirm that a small increase in the density of sintered samples significantly increases its strength [14,25]. Since Weibull modulus is a measure of the spread in fracture strength, it is very important as a gauge of mechanical reliability. Generally, when Weibull modulus is large, the variation in strength is small and the reliability of the material is excellent [33]. Weibull modulus may be affected by microstructure (porosity and interparticle necking), powder processing techniques, grain size and shape, and surface finish [33,34]. Weibull plots of the measured strength data, shown in Fig. 5, were used to calculate Weibull modulus. As it can be seen, Weibull modulus of the sample prepared with 1 mol% of nanosized SnO<sub>2</sub> additive is clearly higher than that of the pure sample. In this study, it was shown that Weibull modulus is in agreement with microstructural observations (Fig. 4). In other words, highly uniform microstructure, smaller grain size and higher density can cause higher fracture strength and higher Weibull modulus all as the consequence of the addition of nanosized SnO<sub>2</sub> [35].

Several factors influence the conductivity of sodium beta alumina ceramics including composition, the relative proportion of  $\beta$  and  $\beta''$  phases present and microstructure (grain size, porosity, impurities, etc.) [16]. The Arrhenius plots of the measured ionic conductivity in the temperature range of 200 to 500 °C are shown in Fig. 6. According to these results, the ionic conductivity of the electrolyte was improved in the presence of nanosized SnO<sub>2</sub> sintering aid. Ionic conductivity of the pure sample at 300 °C was  $0.031 \Omega^{-1} \cdot \text{cm}^{-1}$  while for the



Figure 6. The Arrhenius plots of the conductivity versus temperature for the pure sample and the sample prepared with 1 mol% SnO<sub>2</sub>

sample prepared with 1 mol% of nanosized SnO<sub>2</sub> additive it increased to  $0.052 \,\Omega^{-1} \cdot \text{cm}^{-1}$ . The activation energies calculated for the measured conductivity of the pure sample and sample prepared with 1 mol% of nanosized SnO<sub>2</sub> additive were 0.31 and 0.35 eV, respectively. The smaller grain size and higher grain-boundary volume in the sample with 1 mol% of SnO<sub>2</sub> can be considered as a reason for its higher activation energy [36,37]. Since the Arrhenius plots of the conductivity data tend to converge at low temperatures (Fig. 6), it can be suggested that the effect of nanosized SnO<sub>2</sub> additive is manif ested in the bulk resistance. The conversion to  $\beta''$ -Al<sub>2</sub>O<sub>3</sub> phase can have the most pronounced effect in increasing the ionic conductivity (even up to factors of 4 to 5) [16,17]. Therefore, with the addition of nanosized SnO<sub>2</sub> sintering aid, the lower sodium loss, higher amount of  $\beta''$ -Al<sub>2</sub>O<sub>3</sub> phase and higher density may lead to the decrease in bulk resistance and thus increase ionic conductivity.

#### **IV.** Conclusions

In this study, the effect of nanosized  $\text{SnO}_2$  additive as sintering aid on the properties and microstructure of sodium beta alumina ceramics, synthesized by the solid state process, has been investigated. The results indicated that the addition of 1 mol% of nanosized  $\text{SnO}_2$ decreases sintering temperature of sodium beta alumina ceramics for about 100 °C, increases the percentage of  $\beta''-\text{Al}_2\text{O}_3$  phase from 95% to 99% and improves uniformity of microstructure. As a result, both the fracture strength and the ionic conductivity of the sample are also improved effectively.

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